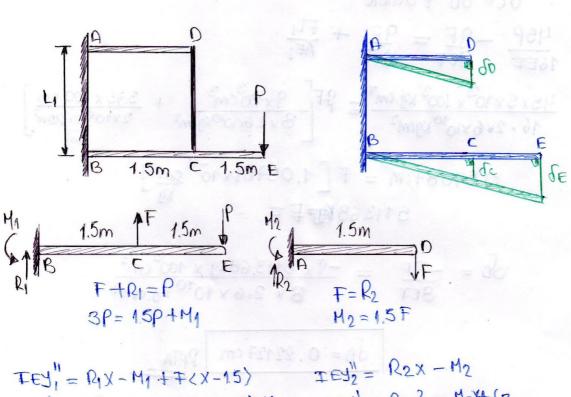


SINGULARIDOS - Superposición

Dos nigas en cantilenver AD y BE de igual ngidez a la flexión $EI = 2.6 \times 10^{10} \, \text{Kg/km}^2$ estan conectadas por una norvilla de Acero DC fara la qual $EI = 2 \times 10^6 \, \text{Kg/cm}^2$, $AI = 3 \, \text{cm}^2$ y $L_1 = 3.75 \, \text{m}$. Se pide hallar la flecha del voladizo en "D" debido a la fuerza $P = 5 \, \text{TN}$.



$$TEY'_{1} = P_{1}X - M_{1} + \mp \langle X - 1.5 \rangle \qquad TEY'_{2} = P_{2}X - M_{2}$$

$$TEY'_{1} = P_{1}X^{2} - M_{1}X + \frac{1}{2} \langle X - 1.5 \rangle + C_{1}X + C_{2} \qquad TEY'_{2} = P_{2}X^{2} - M_{2}X + C_{3}$$

$$TEY_{1} = P_{1}X^{3} - H_{1}X^{2} + \frac{1}{2} \langle X - 1.5 \rangle + C_{1}X + C_{2} \qquad TEY_{2} = P_{2}X^{3} - \frac{M_{2}X^{2}}{6} + \frac{M_{2}X^{2}}{2} + C_{3}X + C_{4}X + C_{4$$

Para
$$x=0$$
 $y_1=0$ $0 = 0$ $x=0$ $y_1=0$ $y_1=0$ $y_1=0$

Para
$$x = 1.5$$
 $y_1 = dc$

$$y_1 = \frac{9R_1}{16E1} - \frac{9M_1}{8E1}$$

$$y_1 = \frac{9P}{16E1} - \frac{9F}{16E1} - \frac{27P}{16E1} + \frac{27F}{16E1}$$

$$d_{C} = \frac{9F}{8EI} - \frac{45P}{16EI}$$

Para
$$x = 0$$
 $y_2 = 0$ $c_4 = 0$
Para $x = 0$ $y_2 = 0$ $c_3 = 0$
Para $x = 15m$ $y_2 = d_0$
 $y_2 = \frac{qR_2}{16EI} - \frac{qM_2}{8EI}$
 $y_2 = \frac{qF}{16EI} - \frac{27F}{16EI}$

$$\delta c = \frac{9F}{16EI} - \frac{45P}{16EI} - \frac{9F}{8EI} - \frac{9F}{8EI}$$

$$\delta 0 = -\frac{9F}{8EI}$$

$$\delta 0 = \frac{9F}{8EI}$$

$$\delta 0 = \frac{9F}{8EI}$$

$$do = -\frac{9F}{8EI} = \frac{-9 \times 5113.68 \text{ kg} \times 100^3 \text{ cm}^3}{8 \times 2.6 \times 10^{10} \text{ kg cm}^2}$$

So = 0.22127 cm RptA

Total X=15 Apr Jo.

La viga ABC tiene una rigidez a la flexión EI y una longitud L.
EL extremo c esta unido a un resorte de constante K. determinar la fuerza en el resorte debido al momento aplicado en A.

29ET WET BET SHET SET .

$$TEY' = RAX - M - RB(X - \frac{L}{2})$$

$$TEY' = RAX^{2} - MX - RB(X - \frac{L}{2})^{2} + C_{1}$$

$$TEY' = RAX^{3} - MX^{2} - RB(X - \frac{L}{2})^{3} + C_{1}X + C_{2}$$

Pora
$$X=0$$
 $C_2=0$

Para $X=\frac{1}{2}$ $Y=0$
 $C_1=\frac{ML}{4}-\frac{RAL^3}{2H}$

$$TEY = \frac{RAL^3 - RBL^3 - ML}{48}$$

$$TEY = \frac{Fl^3 + Ml^2 - Fl^3 - Ml^2 - Ml^2}{9}$$

$$Tey = \frac{Fl^3}{12} - \frac{Hl^2}{24}$$

$$y = -\left[-\frac{FL^3}{12ET} + \frac{ML^2}{24ET} \right]$$

$$y = \frac{Ml^2}{24Er} - \frac{FL^3}{12Er}$$

$$\frac{F}{K} + \frac{FL^3}{12EI} = \frac{ML^2}{24EI}$$

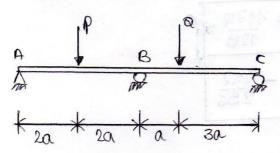
$$F \left[\frac{12EI + KL^3}{12KEI} \right] = \frac{ML^2}{24EI}$$

$$F = \frac{K ML^2}{24EI}$$

$$24EI + 2KL^3$$

SINGULARIDAD

Para la mga ABC mostrada, donde EI es constante, déterminar la relación entre Las fuerzas Py Q, pora la fuerza cortante en "c" spa siempre negativa.



$$TEY'' = RAX - P(X-20) + RB(X-40) - Q(X-50)$$

$$TEY' = \frac{RAX^{2}}{2} - \frac{P(X-20)^{2} + \frac{RB}{2}(X-40)^{2} - Q(X-50)^{2} + C_{1}}{2}$$

$$TEY = \frac{RAX^{3}}{6} - \frac{P(X-20)^{3} + \frac{RB}{6}(X-40)^{3} - Q(X-50)^{3} + C_{1}X+C_{2}}{6}$$

Para
$$x=0$$
 $y=0$ $c_{2}=0$
Para $x=4a$ $y=0$ $c_{1}=?$

$$0 = \frac{32RA}{3}a^3 - \frac{4P}{3}a^3 + C_1(4a)$$

$$c_1 = \frac{\rho}{3} a^2 - \frac{\rho \rho}{3} a^2$$

Para X=8a Y=0

$$0 = \frac{256RAa^3}{3} - \frac{36Ra^3}{3} + \frac{32RBa^3}{3} - \frac{9Qq^3}{2} + \frac{8Ra^3}{3} - \frac{64RAa^3}{3}$$

ESTATICA

$$(\mathbf{I})$$
 – (\mathbf{I})

$$\frac{64RB}{3} - \frac{44P}{3} - \frac{39Q}{2} = 0$$

$$RB = \frac{11P}{16} + \frac{117Q}{128}$$

$$RA = \frac{13P}{128} - \frac{21Q}{128}$$

ESTATICA

$$Rc = \frac{43Q}{256} - \frac{3P}{32}$$

$$\frac{430}{256} - \frac{3p}{32} > 0$$

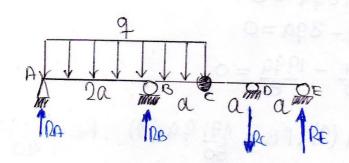
$$\frac{43Q}{256} > \frac{3P}{32}$$

$$\frac{43}{24}$$
 > $\frac{P}{Q}$ R

RPTA

8(a) + 4(a) - 6(a) - 300 = 0

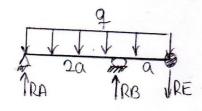
Conouendo q, E, q, e I; calcular la deflexión bajo la rótula



$$3RA + RB = 4.59a$$

$$2RE = RC$$

$$RA+RB - RE = 39a$$



$$IEY'' = RAX - \frac{1}{2}X^2 + RB < X-20$$

Para
$$x=0$$
 $y=0$ $c_2=0$
Para $x=2a$ $y=0$ $c_1=?$

$$0 = 8 \frac{164}{6} a^{3} - \frac{164}{24} a^{4} + 206$$

$$c_{1} = \frac{164}{48} a^{3} - \frac{810}{12} a^{2}$$

$$EIY_1 = \frac{5RA}{2}a^3 + \frac{RBa^3}{6} - \frac{19}{8}4a^4$$

$$0 = \frac{\text{Re}\,a^3}{6} + c_3 a + c_4$$

Para
$$x = 2a$$
 $y = 0$

$$0 = \frac{8RE}{6} a^3 - \frac{Rc}{6} a^3 + 2a(3 + c4)$$

$$c_3 = -\frac{5RE0^2}{6}$$

$$c_4 = \frac{2RE0^3}{3}$$

$$Sara X=0 \quad y_2 = y_1$$

$$\frac{7}{2} = \frac{19}{6} = \frac{19}{3} =$$

May 1000

$$3RA + RB - 4.5qa = 0$$

$$RA + RB - RE - 3qa = 0$$

$$\frac{5RA + RB - 2RE - 19qq = 0}{8} = 0$$

$$RA = \frac{63}{80} 9a (1) RB = \frac{171}{80} 9a (1) RE = \frac{39a}{40} (1)$$

deflexión rótula

$$dc = \frac{2RE}{3EI}q^3$$

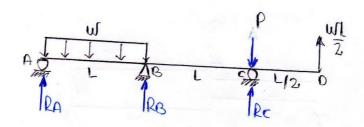
$$\delta c = +\frac{2}{3ET} \left(-\frac{399}{40} \right) a^3$$

$$\delta c = -\frac{4a^4}{20EI}$$

$$\delta c = \frac{40^{\circ}}{20ET} (1)$$

RPTA.

comprobado por Áreo de momento Utilizando el método funciones de singularidad, cal whar los momentos en los apoyos y las reactiones. dibujor los diagramos de DFC y DMF.



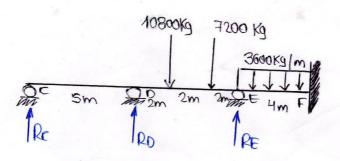
$$\begin{aligned} \text{TEY}^{11} &= \text{RAX} - \frac{\omega x^{2}}{2} + \text{RB} \langle x - L \rangle + \frac{\omega \langle x - L \rangle^{2}}{2} - \frac{\rho \langle x - 2L \rangle}{2} + \frac{\rho \langle x$$

Para
$$x=0$$
 $y=0$ $c_2=0$
Para $x=1$ $y=0$ $c_1=\frac{W1^3}{24}$ Rate

$$M_{c=0}$$
 $0 = 2RA + RB - \frac{7}{4}WL$
 00 $RA = \frac{3}{8}WL$

$$c = c - \frac{1}{2} M c$$

Para la viga cargada como se indica, détermine los DFC y DMF. Aplique el método de funciones de singularidad. EI = ete



 $\begin{aligned} \mathbf{TEY}'' &= & \text{Rex} + \text{Ro}\langle x-5\rangle - 10800\langle x-7\rangle - 7200\langle x-9\rangle + \text{Re}\langle x-11\rangle - 3600\langle \underline{x-13}\rangle^2 \\ \mathbf{TEY}' &= & \text{Rex}^2 + \frac{\text{Ro}}{2}\langle x-5\rangle^2 - 5400\langle x-7\rangle^2 - 3600\langle x-9\rangle^2 + \frac{\text{Re}}{2}\langle x-11\rangle^2 - 600\langle x-13\rangle^2 + C_1 \\ \mathbf{TEY} &= & \text{Rex}^3 + \frac{\text{Ro}}{6}\langle x-5\rangle^3 - 1800\langle x-7\rangle^3 - 1200\langle x-9\rangle^3 + \frac{\text{Re}}{6}\langle x-11\rangle^3 - 150\langle x-13\rangle + C_1 \\ \mathbf{TEY} &= & \text{Rex}^3 + \frac{\text{Ro}}{6}\langle x-11\rangle^3 - 150\langle x-13\rangle + C_1 \\ \mathbf{TEY} &= & \text{Rex}^3 + \frac{\text{Ro}}{6}\langle x-11\rangle^3 - 150\langle x-13\rangle + C_1 \\ \mathbf{TEY} &= & \text{Rex}^3 + \frac{\text{Ro}}{6}\langle x-11\rangle^3 - 150\langle x-13\rangle + C_1 \\ \mathbf{TEY} &= & \text{Rex}^3 + \frac{\text{Ro}}{6}\langle x-11\rangle^3 - 150\langle x-13\rangle + C_1 \\ \mathbf{TEY} &= & \text{Rex}^3 + \frac{\text{Ro}}{6}\langle x-11\rangle^3 - 150\langle x-13\rangle + C_1 \\ \mathbf{TEY} &= & \text{Rex}^3 + \frac{\text{Ro}}{6}\langle x-11\rangle^3 - 150\langle x-13\rangle + C_1 \\ \mathbf{TEY} &= & \text{Rex}^3 + \frac{\text{Ro}}{6}\langle x-11\rangle^3 - 150\langle x-13\rangle + C_1 \\ \mathbf{TEY} &= & \text{Rex}^3 + \frac{\text{Ro}}{6}\langle x-11\rangle^3 - 150\langle x-13\rangle + C_1 \\ \mathbf{TEY} &= & \text{Rex}^3 + \frac{\text{Ro}}{6}\langle x-11\rangle^3 - 150\langle x-13\rangle + C_1 \\ \mathbf{TEY} &= & \text{Rex}^3 + \frac{\text{Ro}}{6}\langle x-11\rangle^3 - 150\langle x-13\rangle + C_1 \\ \mathbf{TEY} &= & \text{Rex}^3 + \frac{\text{Ro}}{6}\langle x-11\rangle^3 - 150\langle x-13\rangle + C_1 \\ \mathbf{TEY} &= & \text{Rex}^3 + \frac{\text{Ro}}{6}\langle x-11\rangle^3 - 150\langle x-13\rangle + C_1 \\ \mathbf{TEY} &= & \text{Rex}^3 + \frac{\text{Ro}}{6}\langle x-11\rangle^3 - 150\langle x-13\rangle + C_1 \\ \mathbf{TEY} &= & \text{Rex}^3 + \frac{\text{Ro}}{6}\langle x-11\rangle^3 - 150\langle x-13\rangle + C_1 \\ \mathbf{TEY} &= & \text{Rex}^3 + \frac{\text{Ro}}{6}\langle x-11\rangle^3 - 150\langle x-13\rangle + C_1 \\ \mathbf{TEY} &= & \text{Rex}^3 + \frac{\text{Ro}}{6}\langle x-11\rangle^3 - 150\langle x-13\rangle + C_1 \\ \mathbf{TEY} &= & \text{Rex}^3 + \frac{\text{Ro}}{6}\langle x-11\rangle^3 - 150\langle x-13\rangle + C_1 \\ \mathbf{TEY} &= & \text{Rex}^3 + \frac{\text{Ro}}{6}\langle x-11\rangle^3 - 150\langle x-13\rangle + C_1 \\ \mathbf{TEY} &= & \text{Rex}^3 + \frac{\text{Ro}}{6}\langle x-11\rangle^3 - 150\langle x-13\rangle + C_1 \\ \mathbf{TEY} &= & \text{Rex}^3 + \frac{\text{Ro}}{6}\langle x-11\rangle^3 - 150\langle x-13\rangle + C_1 \\ \mathbf{TEY} &= & \text{Rex}^3 + \frac{\text{Ro}}{6}\langle x-11\rangle^3 - 150\langle x-13\rangle + C_1 \\ \mathbf{TEY} &= & \text{Rex}^3 + \frac{\text{Ro}}{6}\langle x-11\rangle^3 - 150\langle x-13\rangle + C_1 \\ \mathbf{TEY} &= & \text{Rex}^3 + \frac{\text{Ro}}{6}\langle x-11\rangle^3 - 150\langle x-13\rangle + C_1 \\ \mathbf{TEY} &= & \text{Rex}^3 + \frac{\text{Ro}}{6}\langle x-11\rangle^3 - 150\langle x-13\rangle + C_1 \\ \mathbf{TEY} &= & \text{Rex}^3 + \frac{\text{Ro}}{6}\langle x-11\rangle^3 - 150\langle x-13\rangle + C_1 \\ \mathbf{TEY} &= & \text{Rex}^3 + \frac{\text{Ro}}{6}\langle x-11\rangle^3 + C_1 \\ \mathbf{TEY} &= & \text{Rex}^3 + \frac{\text{Ro}$

Para $x=0 \ y=0 \ c_2=0$

fara $X=5 Y=0 C_{1}=-\frac{25}{6}Rc$

Para X=11 Y=0 0 = 44Rc +9RD -31200

Para x=15 y'=0 0=325Rc +150R0 +24R€-1940000

Para X=15 y=0 0=375Rc +125Ro +8RE -887400

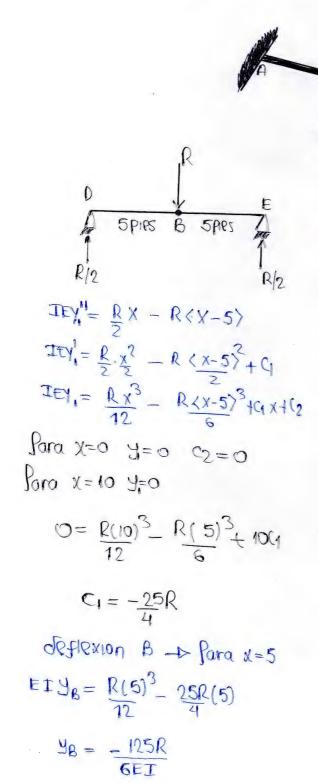
RC = - 1474 Kg

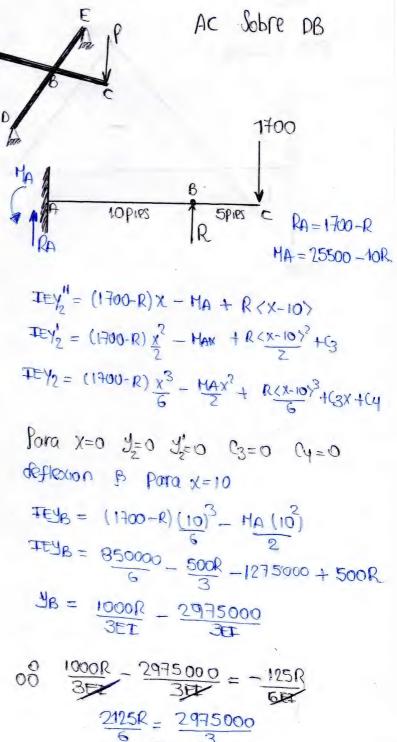
RD = + 10672.89

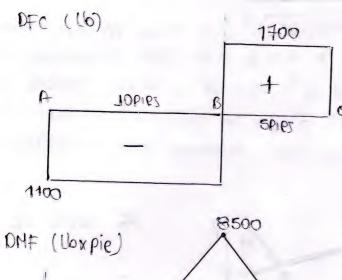
RE=+ 13254. 86

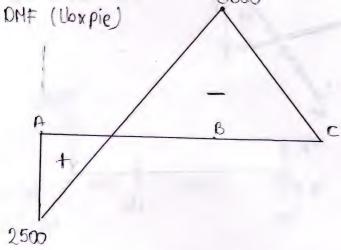
Singulandod

La viga ABE esta empotrada en "A" y se apoya en el punto medio de la viga DE. Lo distonua de A a B es de 10 pies, la distancia de B a C es 5 pies y la longitud de la viga DE es 10 pies, ambas vigas tienen la misma rigidez (EI). dibujar los diagramas de fuerza cortonte y momento flector de la viga ABC, sobiendo que P = 1700 Libras.

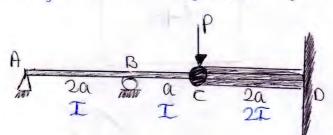


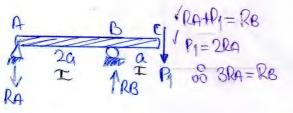






La viga ABCD mostrada, tiene una rótula en c y esta empotrada en D. utilizando el método de funciones de singularidad, dibujar los diagramas de fuerza cortante y momento fledor.





RA

$$IRS$$
 IRS
 IRS

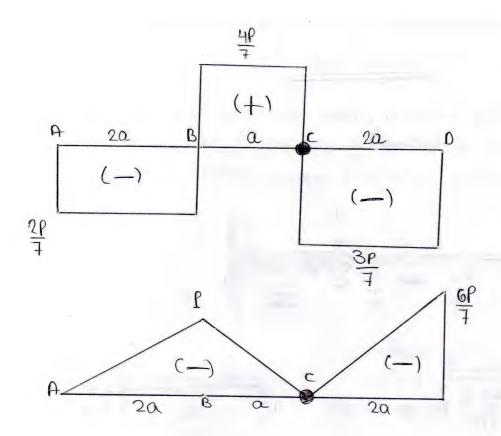
$$0 = - PA(20)^{3} + CI(20)$$

$$C_1 = \frac{2 \ln \alpha^2}{3}$$

Para x = 2a $y_2' = 0$ $c_3 = +2f_2q^2$ Para x = 2a $y_2 = 0$ $c_4 = -\frac{8f_2}{3}q^3$

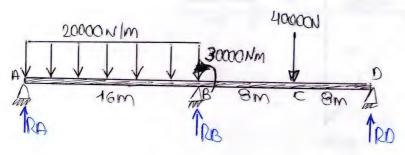
$$\frac{1}{2}RA = P$$
 $RA = 2$

$$RA = \frac{2P}{7}(1)$$
 $RB = \frac{6P}{7}(1)$ $RD = \frac{3P}{7}(1)$ $M = \frac{6P}{7}(1)$



SINGULARIDAD

La viga mostrada Tiene EI = cte. Dibyjar el diagrama de fuerza cortante y momento flector



 $IEV' = \frac{2000}{5} \times -\frac{40000}{5} \times -\frac{8}{5} + \frac{30000}{5} \times -\frac{16}{7} + \frac{1}{16} \times -\frac{16}{7} - \frac{20000}{5} \times \frac{16}{7} = \frac{2000}{3} \times -\frac{16}{7} + \frac{2500}{3} \times -\frac{16}{7} +$

Para x=16m y=0

$$0 = \frac{204880 - 10240000 + 164}{3}$$

$$C_1 = 640000 - 128 RD$$

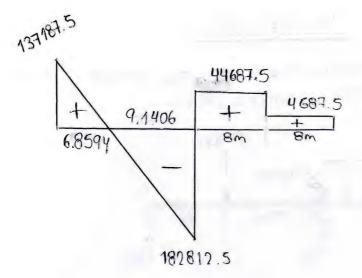
. Para X=32 4=0

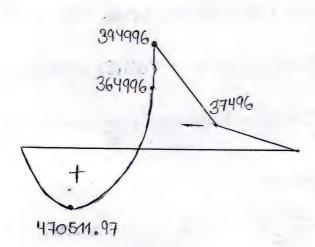
$$0 = \frac{16384R0}{3} - 92160000 + 3840000 + \frac{2048RB}{3} - \frac{16384000}{3} + 3204$$

$$0 = 4096120 + 204818 - 136106666.7$$

ESTATICA

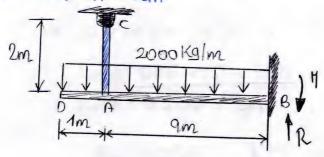
$$R0 = -9687.5$$





Singulandad

Pora el sistema mostrado, formado por una viga (DAB) y un cable (CA) ambos de acero ($E=2\times10^6\,\text{Kg}\,\text{cm}^2$). Se soliuta dibujar los diagramas de fuerza cortante y momento flector de la niga DAB, sabiendo que pora la niga $I=500\,\text{cm}^4$ y para el cable $I=500\,\text{cm}^4$



$$c_1 = \frac{2000(10^3)}{6} - \frac{F(9)^2}{2}$$

$$C_1 = \frac{1000000}{3} = \frac{81F}{2}$$

Sara $X=10$ $Y=0$

$$0 C_2 = \frac{2000(10)^4}{24} - \frac{F(9)^3}{6} - \frac{10000000 \times 10}{3} + \frac{810}{2}F$$

$$C_2 = \frac{567F}{2} = 2500000$$

Jeflexion en la mga

Para
$$X_1 = Y = ?$$

IEY = $-2000 + 10^6 - 81F + 567F - 2500000$

IEY = $243F - 2166750$ m³

 $Y = 243F - 2166750$ Kgm³

 $2x10^{10}x 500x 16^8$ Kgm²

 $Y = 243F - 2166750$ m°

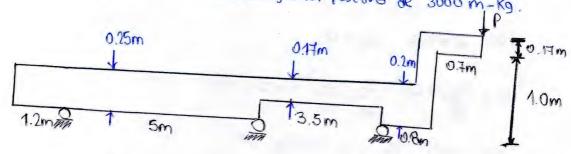
Jeflexion en la barra

 $S = \frac{Fx}{5x10^4}x 2x10^{10}$
 $S = \frac{Fx}{5x10^4}x 2x10^{10}$
 $S = \frac{243F}{5x10^4}x 2x10^{1$

10957.64

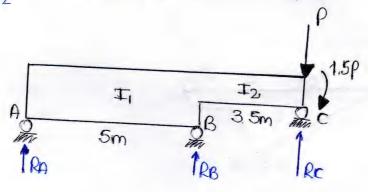
SINGULARINAD

En la viga mostrada, se pide determinar el valor que debe tener la fuerza Puntual "p", aplicada en el extremo del volado, de manera que en el apoyo "B" se genere un momento fledor positivo de 3000 m-Kg.



$$T_1 = \frac{1 \text{m} \times 0.25 \text{ m}}{12} = 1.302 \times 10^{-3} \text{m}^4$$

$$T_2 = \frac{1m \times 0.17m}{12} = 4.094 \times 10^{-4} \text{ m}^4$$



$$T_1 = RAX$$
 $T_1 = S_1 = RAX^2 / 2 + C = 0$
 $T_1 = S_1 = RAX^3 / 6 + C / X + C / 2$

Para
$$x=5$$
 $y_1=0$

$$0 = \frac{RAx^3 + CIX}{6}$$

$$\frac{-25RA = CI}{6}$$

$$T_2 E y_2'' = RAX + RB < X-5$$

 $T_2 E y_2' = RAx^2 / 2 + RB < X-5)^2 / 2 + C_3$
 $T_2 E y_2' = RAx^3 / 6 + RB < X-5)^3 / 6 + C_3 X + C_4$

Cy = 28.562 RA

Para
$$x = 5$$
 $y_2 = 0$

$$0 = \frac{Rax^{3}}{6} + \frac{C3x + C4}{5}$$

Para $x = 5$ $y'_{1} = y'_{2}$

$$Rax^{2} + c_{1} = \frac{I_{1}}{I_{2}} \left(\frac{Rax^{2}}{2} + c_{3} \right)$$

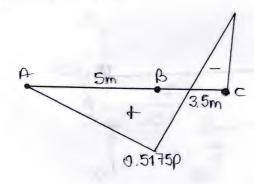
$$\frac{2500}{2} - \frac{2500}{6} = 3.18(\frac{2500}{2}) + 3.1863$$

$$C_3 = -9.879$$
 .

· De la establa

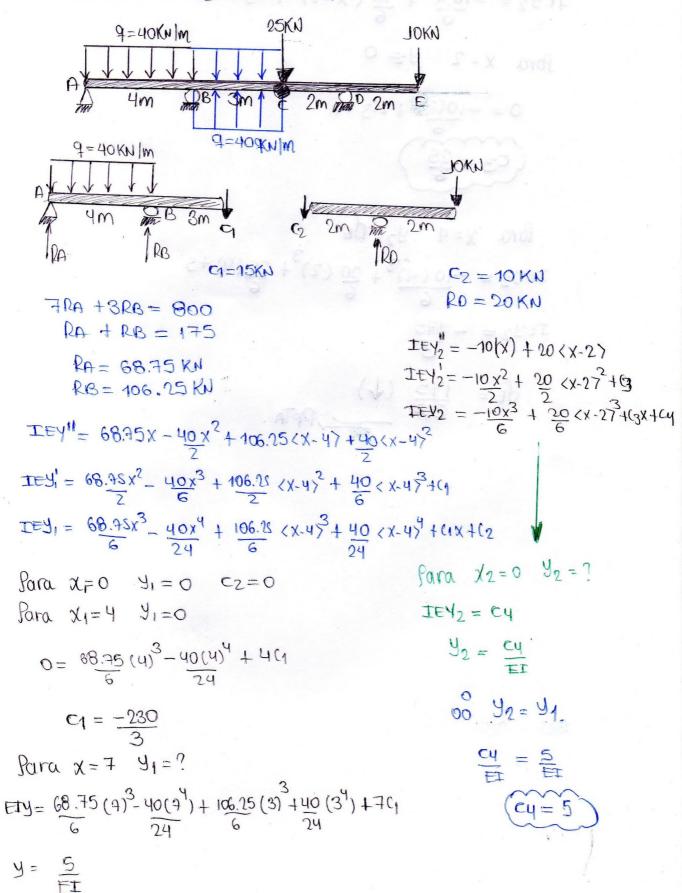
Para
$$x = 8.5$$
 $y_2 = 0$

$$0 = \frac{\Omega \Omega}{8} (8.5)^3 + \frac{\Omega B}{6} (3.5)^2 + 8.5 (3 + 4)$$



$$0.5175p = 3000 \text{ m-Kg}$$

DETERMINAR la deflexión en el punto E de la mga mostrada



$$TEY_2 = -\frac{10}{6}x^3 + \frac{20}{6}(x-2)^3 + \frac{20}{6}(x+2)^4 + \frac{20}$$

$$0 = -10(2)^3 + 2(3 + 5)$$

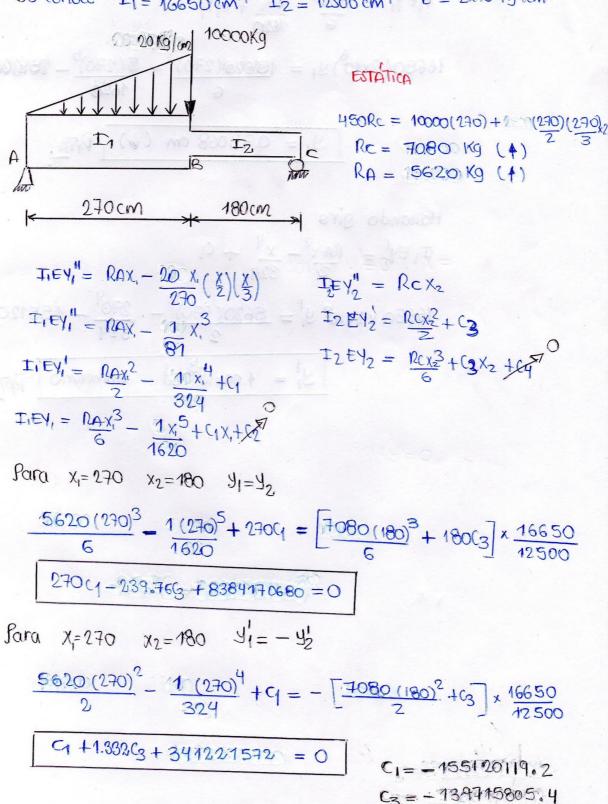
$$\left(c_3 = \frac{25}{6}\right)$$

$$IEY_2 = -\frac{10(4)^3}{6} + \frac{20}{6}(2)^3 + \frac{25(4)}{6}(4) + 5$$

$$IEY_2 = -\frac{175}{3}$$

FUNCION DE SINGULARIDAD

Dada la viga simplemente apoyada de momento de inercia varieble, determine el gira y la flecha en el punto de la carga aplicada de lotar par el método de funciones de singularidad. Se conoce $I_1 = 16650 \, \text{cm}^4$ $I_2 = 12500 \, \text{cm}^4$ $I_3 = 2 \times 10^6 \, \text{kg} \, \text{lcm}^2$



Hollando deflexión

$$I_1 = \frac{RAx^3}{6} - \frac{9x_1^5}{1620} + 9x_1$$

$$16650(2\times10^{6})y_{1} = \frac{15620(270)^{3}}{6} - \frac{(270)^{5}}{1620} - \frac{155120719.2(290)}{1620}$$

Hallando giro 2008

$$I_1 EY'_1 = \frac{\Omega A x^2 - x^4}{20} + C_1$$

$$16650 \times 2 \times 10^{6} \text{ y}_{1}^{1} = \frac{5620(270)^{2} - \frac{270^{4}}{324} - 155120119.2$$

$$y'_1 = 1.00 \times 10^3 \text{ rad}$$
 antihorario RPTA

fora X=270 xz=180 41=-4

- = 15 + (045)00h - (043)000 046